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L2	204	703/10.ccls.	US-PGPUB; USPAT; EPO; JPO; DERWENT; IBM_TDB	OR	ON	2006/02/27 14:30
L3	3471	reservoir with permeability	US-PGPUB; USPAT; EPO; JPO; DERWENT; IBM_TDB	OR	ON	2006/02/27 14:15
L4	95	L3 and (saturation with distribution)	US-PGPUB; USPAT; EPO; JPO; DERWENT; IBM_TDB	OR	ON	2006/02/27 14:15
L5	28	L4 and (flow with (model\$5 or simulat\$5 or emulat\$5))	US-PGPUB; USPAT; EPO; JPO; DERWENT; IBM_TDB	OR	ON	2006/02/27 14:15
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Critical Evaluation of the Ensemble Kalman Filter on History Matching of Geologic Facies

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In this paper, the distributions of reservoir-model realizations from 20 independent ensembles are compared with the distributions from 20 randomized-maximum-likelihood (RML) realizations for a 2D waterflood model with one injector and four producers. A secondary objective of history matching is often to assess the uncertainty in the predictions of future reservoir performance or in the estimates of reservoir properties such as permeability, porosity, or saturation. A facies type can be attributed to each region, so up to seven different kinds of facies can be modeled with appropriate relative percentage.

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Effect of Oil Production Rate on Performance of Wells Producing from More Than One Horizon

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A Comparison of Calculated krg/kro Ratios With a Correlation of Field Data

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Formulation of Capillary Force Barriers in Moderately-Oil Wet Systems and Their Application to Reservoir Simulation

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There are some discussions available about this issue in the literature.⁷ Hysteresis of Relative Permeability. 14) On the basis of Eqs. 7 through 11, the relative permeability in hysteresis, as well as the capillary pressure, can be derived mathematically.^{4,6,8} Examples of This Formulation. Then, the calculated imbibition capillary pressures and primary imbibition relative permeability curves can be created, as demonstrated in

Figs. 3 through 6, where IAH is controlled by the appropriate X and Y values. Additionally, it is clear that imbibition capillary pressure and relative permeability are strongly controlled by wettability.

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Extended Brigham Model for Residual Oil Saturation Measurement by Partitioning Tracer Tests

SPE eLibrary In spite of its limitations, the model is useful in estimating layer heterogeneity, layer distribution, per- meability contrast, and dispersion in the reservoir. Introduction Interwell tracer testing has been recognized as a reliable method for determining residual oil saturation between wells. In the model, flow distribution is gov- erned by the weighted permeability-thickness of the layers (Eq. 5) and the produced tracer concentration is obtained by summing the production from all layers (Eq. 6). $q_j = 1 N K_{rw,j} h_j$

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A New Model To Obtain Representative Field Relative Permeability for Reservoirs Produced Under Solution-Gas Drive

SPE eLibrary Français du Pétrole (IFP) Summary Relative permeability curves (k_r) control production and are of primary importance for any type of recovery process. We have developed a novel approach for calculating represen- tative field relative permeabilities. Relative permeabilities are de- rived from these "numerical" experiments in the same way as they are from real experiments. In the literature, two main types of ap- proaches are currently used to interpret the laboratory data in terms of relative permeability.

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Prediction of Wettability Variation Within an Oil/Water Transition Zone and Its Impact on Production

SPE eLibrary Masalmeh4 measured oil relative permeability in cores that had been aged at different initial water saturations. He found that the oil relative permeability at a given water saturation increased with initial wa- ter saturation (increasingly water-wet conditions). Consequently, the initial water saturation and production behavior is different depending on whether wettability alteration has occurred. At each step, water and oil saturations, relative permeabilities, and the capillary pressure are calculated subject to pressure boundary conditions at the inlet and outlet faces, and periodic boundaries on the other faces.

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Methodology for Numerical Simulation With Cycle-Dependent Relative Permeabilities

SPE eLibrary In particular, relative permeabilities are considered to be dependent on saturation and saturation history. Theoretical Approach Relative permeabilities are generally regarded as saturation depen- dent, and three-phase relative permeabilities are described as func- tions of one- or two-phase saturations. Alternative types of functional representations among relative permeability, saturations, and initial saturation point are presented in this section. Like the two-phase hysteresis models, the three-phase models use relative permeabilities for one type of saturation di- rection to estimate permeabilities for another saturation direction.

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Engineering Core Analysis

SPE eLibrary However, if determination of endpoint saturations is one of the objectives, a coring fluid is designed to maintain the immobile-phase saturation. If a core is to be used to define fluid- saturation-dependent parameters, such as relative permeability, capillary pressure, or electrical properties, the drilling fluid should be formulated to maintain core-wettability characteristics as they were in the reservoir. Fluid saturations, porosity, and absolute permeabili- ty are determined. Measured gas permeability can be quite different from the liquid permeability in a variety of samples, especially those with shales and clays.

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Estimating Permeability by Use of Neural Networks in Thinly Bedded Shaly Gas Sands

SPE eLibrary Among other factors, rock wettability controls the distribution and relative permeability of those fluids, as well as electrical properties of the containing rocks. Measurement of irreducible water saturation, S_{wi} , and computation of wettability together with permeability measurements can define flow units, suggest which ones to produce and in what order, and help generate enhanced recovery programs. Recently, wireline NMR tool measurements have changed permeability evaluation by providing continuous data that is directly related to in-situ permeability. This third method used NMR echoes to match Klinkenberg permeability.

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Experimental Study of Gas Slippage in Two-Phase Flow

SPE eLibrary The gas relative permeabilities have been measured at different mean pore pressures, and the values of two-phase gas slip factors have been computed at different water saturations. If the slip effect is not considered correctly, the gas relative permeabilities will vary with test pressures and may be greater than 1 at some water saturations. In this paper, gas/liquid relative permeabilities were measured at different pressures. 8) where $k_{rg}(S_w, p_m)$ is the relative permeability of the gas phase at a water saturation of S_w and a mean pressure of p_m , and k is the absolute permeability of the rock sample measured by liquid injection.

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Sand-Production Simulation in Heavy-Oil Reservoirs

SPE eLibrary A stable production period with enlarged cavities, when the damaged zone and the permeability impairment have been removed. First, water influx implies increasing water saturation; this leads to a reduction in capillary cohesion. When water influx starts, capillarity is destroyed as water saturation rises. Second, water influx and saturation changes also imply relative permeability changes in the near-wellbore region; this alters the pressure distribution and, therefore, the effective stresses, processes which lead to cohesion loss and sand failure.

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Effect of Crossflow on Foam-Induced Diversion in Layered Formations

SPE eLibrary In stratified formations with damaged intervals distributed along the wellbore, the acidizing treatment often results in acid loss into nondamaged zones (high permeability), leading to a nonuniform injection profile. In the first stage, foam is placed in high-permeability layers (foam placement). Rossen¹³ and later Tanzil et al.¹⁴ proved theoretically that foam generation is promoted as gas flows from low permeability to high permeability. 2) where H_{r,N_2} and $H_{r,s}$ are CT values of nitrogen-saturated rock and surfactant solution-saturated rock, respectively.

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Simultaneous Gravel Packing and Filter-Cake Cleanup With Shunt Tubes in Openhole Completions: A Case History From the Gulf of Mexico

SPE eLibrary Additional benefits are associated with their costs relative to cased-hole completions. The upper lobe, 8 ft thick, is very fine-grained with an estimated permeability of 150 md, 60% water saturation, and 6 ft of net gas pay capped by a 2-ft tight streak. The lower lobe is a thick, well-developed sand with an estimated permeability of 1,000 md, 10% water saturation, and 16 ft of net TVT gas pay on water.

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Relative Permeability Correlation for Mixed-Wet Reservoirs

SPE eLibrary Page 1 Relative Permeability Correlation for Mixed-Wet Reservoirs A. Kjosavik and J.K. Ringen, Statoil, and S.M. Skjaeveland, Stavanger U. College Summary A two-phase relative permeability correlation for mixed-wet rock is presented and validated. The well-known Corey-Burdine relative permeabilities were developed for water-wet rock from a Brooks-Corey power-law capillary pressure correlation and a bundle-of-tubes network model. We have extended this correlation to mixed-wet rock and now propose the ensuing relative permeability correlation for mixed-wet reservoirs. The first process will then be primary drainage.

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Multiphase Flow and Drilling-Fluid Filtrate Effects on the Onset of Production

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**An Experimental and Analytical Study of Steam/Water Capillary Pressure****SPE eLibrary**

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**Full-Field Modeling Using Streamline-Based Simulation: Four Case Studies****SPE eLibrary**

Emanuel and Milliken¹ showed how hybrid streamtube models were used to history match field data rapidly to arrive at both an updated geologic model and a current oil-saturation distribution for input to FD simulations. On the other hand, FD simulation is well suited to small models, in which complex surface modeling is required or the details of fluid physics such as high compressibility (live oils, condensates), capillary effects, and relative permeability hysteresis are important.

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**A Literature Analysis of the WAG Injectivity Abnormalities in the CO₂ Process****SPE eLibrary**

The planned WAG ratios of 0.5:4 in frequencies of 0.1 to 2% PV slugs of each fluid¹¹ will cause water-saturation increases during the water cycles and decreasing water saturations during the gas half of the WAG cycle. The validity of this assumption depends on the relative size of the injection cycles. The use of horizontal CO₂ injection wells can increase injection rates several-fold over the injection rates achievable with vertical wells in a five-spot pattern.^{32,33} This is an important consideration in low-permeability reservoirs.

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**Tenth SPE Comparative Solution Project: A Comparison of Upscaling Techniques****SPE eLibrary**

Full details are provided in Appendix A. The permeability distribution is a correlated, geostatistically generated field, shown in Fig. 1. The solutions submitted for the 5 × 5 grid used single-phase upscaling only (Roxar) or single-phase upscaling plus regression-based pseudoization of relative permeabilities (Coats, Phillips, and Landmark). Coats showed that good results also could be obtained with homogeneous absolute permeability and no alteration of relative permeability, and Phillips showed that good results could be obtained from a 6 × 2 grid. Fig. 2—Relative permeabilities for Model 1.

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**Effect of Pore-Lining Chlorite on Petrophysical Properties of Low-Resistivity Sandstone Reservoirs****SPE eLibrary**

The distribution of pore throats is bi- or tri-modal, with a large contribution of microporosity. The values of CEC or SSA are too low to fully explain the low values of the saturation index n . Samples with permeabilities lower than 1 md were discarded. They were then vacuum-saturated with brine, and the brine was flushed at high flow to ensure a good saturation.

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**Pore-Network Model of Flow in Gas/Condensate Reservoirs****SPE eLibrary**

The relative permeabilities and non-Darcy coefficients have been computed for the low capillary number and low condensate saturation-high pressure gradient flow

regimes. Henderson et al.^{4,5} have conducted steady-state relative permeability experiments on model gas-condensate fluids to show that relative permeabilities depend on both saturation and capillary number. The saturation range at which relative permeability was obtained is rather limited. The critical condensate saturation and the relative permeabilities were calculated, but the capillary number effect was not studied.

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... reserves for extended field life ■ Improved input for **reservoir** management ■

Optimized ... Ability to work in all wellbore **fluids** ■ **Dynamic** measurement range ...

www.slb.com/media/services/evaluation/analysis/chfr.pdf - 2004-12-14 - [Text Version](#)

[PDF] MDT Modular Formation Dynamics Tester

... gauges with best-in-class resolution, repeatability and **dynamic** response for ... of the fluid to quantify the amount of **reservoir** and drilling **fluids** in the ...

www.slb.com/media/services/evaluation/reservoir/mdt.pdf - 2004-12-14 - [Text Version](#)

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[PDF] A New Slogan for Drilling Fluids Engineers

... of what are called "drill-in **fluids** ." Most drilling fluid companies have developed drill-in **fluids** to allow effective cleanup following **reservoir** drilling ...

www.slb.com/media/services/resources/oilfieldreview/ors97/spr97/new_slogan.pdf

[PDF] Advanced Fracturing Fluids Improve Well Economics

... in Economides MJ and Nolte KG (eds): **Reservoir Stimu- lation** ... special fluid-loss simulator was designed to prepare the **fluids** under **dynamic** conditions, sub ...
www.slb.com/media/services/resources/oilfieldreview/ors95/aut95/08953451.pdf
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[PDF] CoolFRAC

... probability ■ Minimized damage to **reservoir** and proppant ... guar, low- damage fracturing **fluids** ■ State-of ... Real-time monitoring with **dynamic** decision-making to ...
www.slb.com/media/services/stimulation/fracturing/coolfrac.pdf - 2004-07-15 - [Text Version](#)

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